

STADIUM model

Technical basis

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Cementitious Barriers Partnership

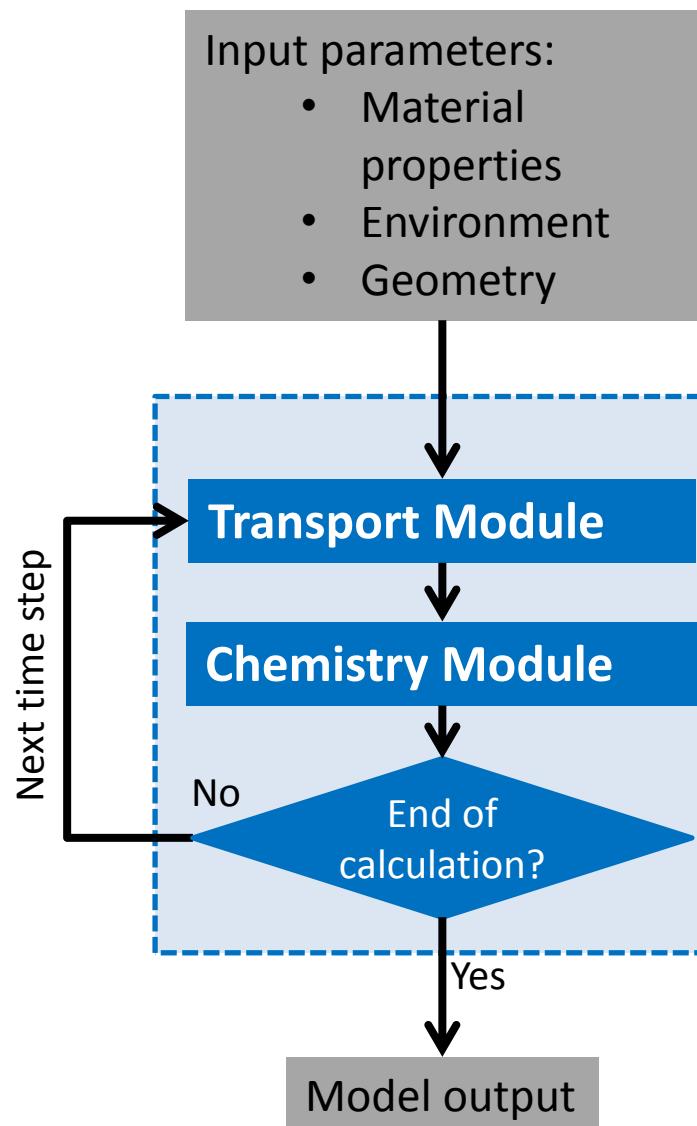
SIMCO Technologies Inc.

August 2014

CBP

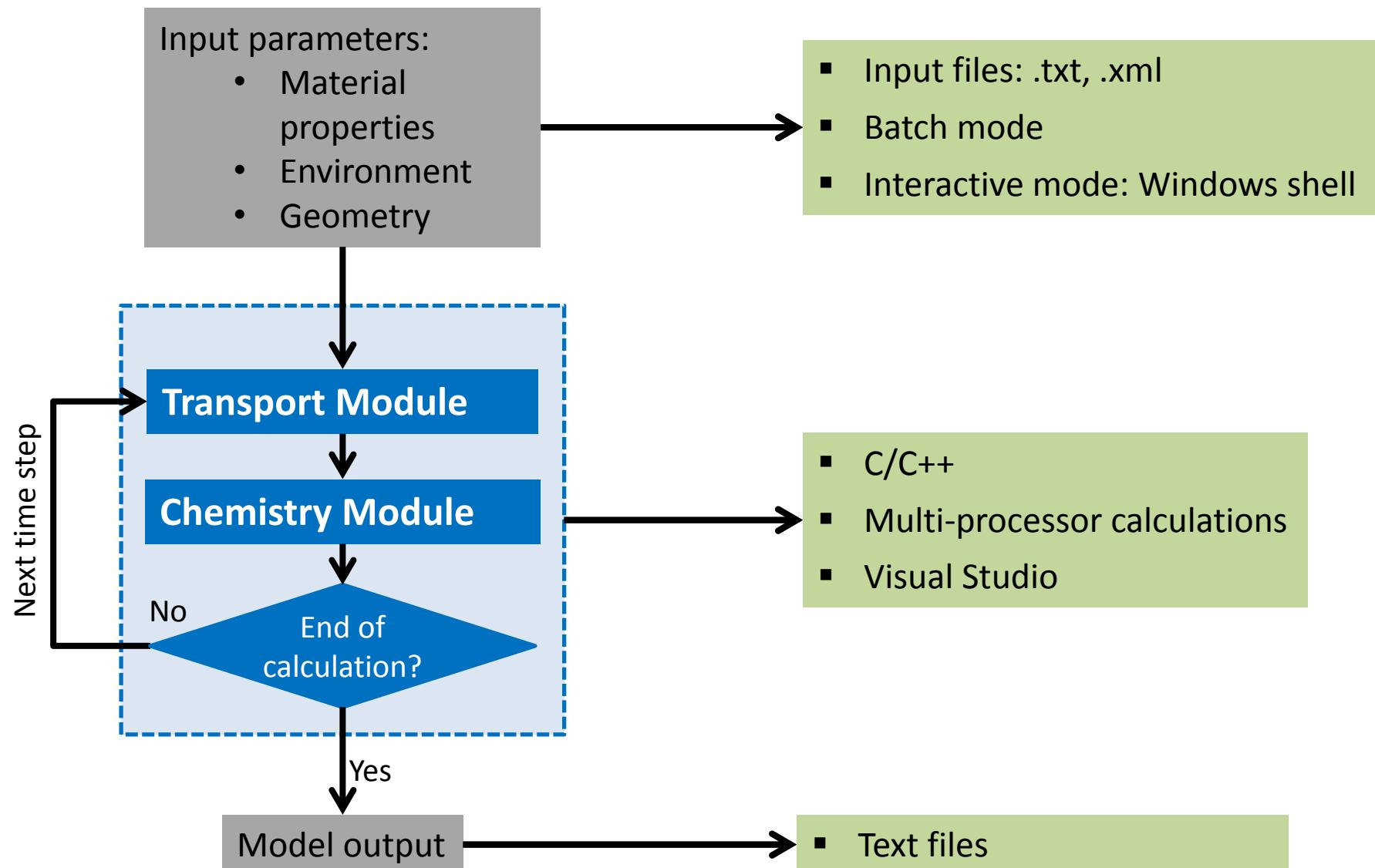
Cementitious Barriers Partnership

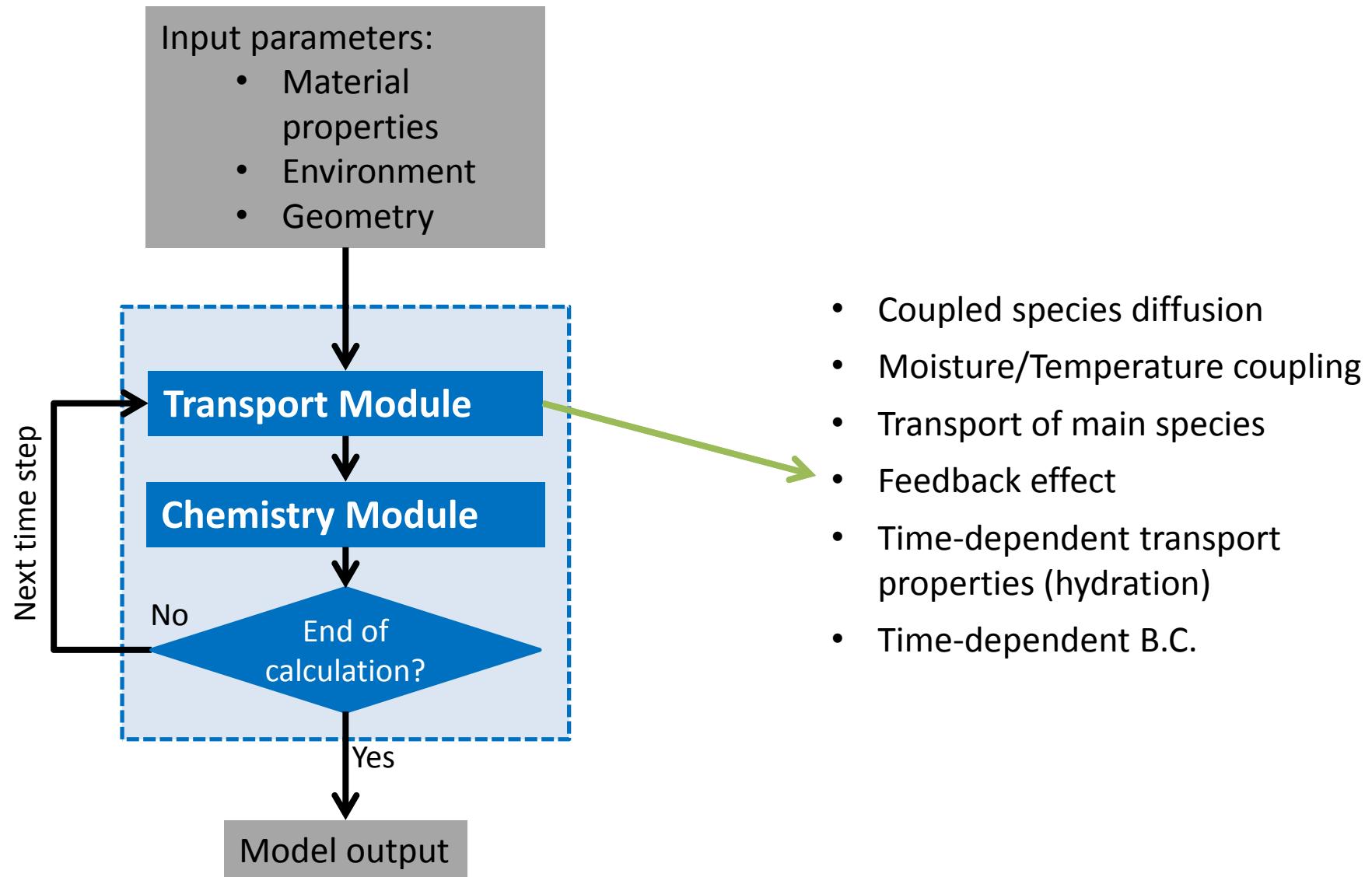


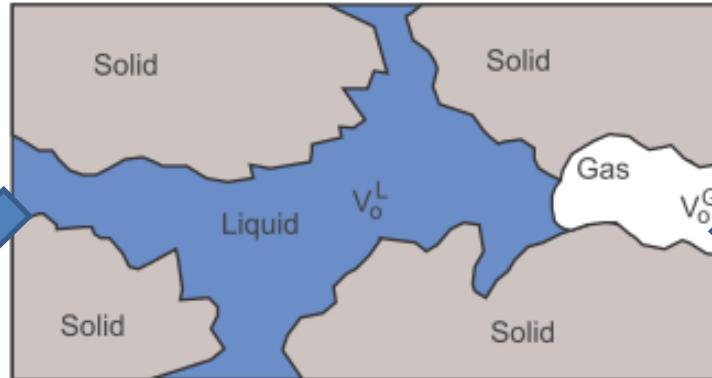


The model is divided in 2 main modules:

- The transport module makes the species move during one time step,
- The chemistry module simulates the reactions between species in the pores and the hydrated paste.







$$\mathbf{v}_l = -\frac{k_l}{\mu} \operatorname{grad}(p_l)$$

$$\mathbf{j}_v = -\theta_g \tau_g D_v^o \operatorname{grad}(\rho_v)$$

Averaging over REV

Assumption: diffusion-only movement of vapor

$$\frac{\partial w}{\partial H} \frac{\partial H}{\partial t} + \frac{\partial w}{\partial T} \frac{\partial T}{\partial t} - \operatorname{div}(D_{mH} \operatorname{grad}(H) + D_{mT} \operatorname{grad}(T)) = 0$$

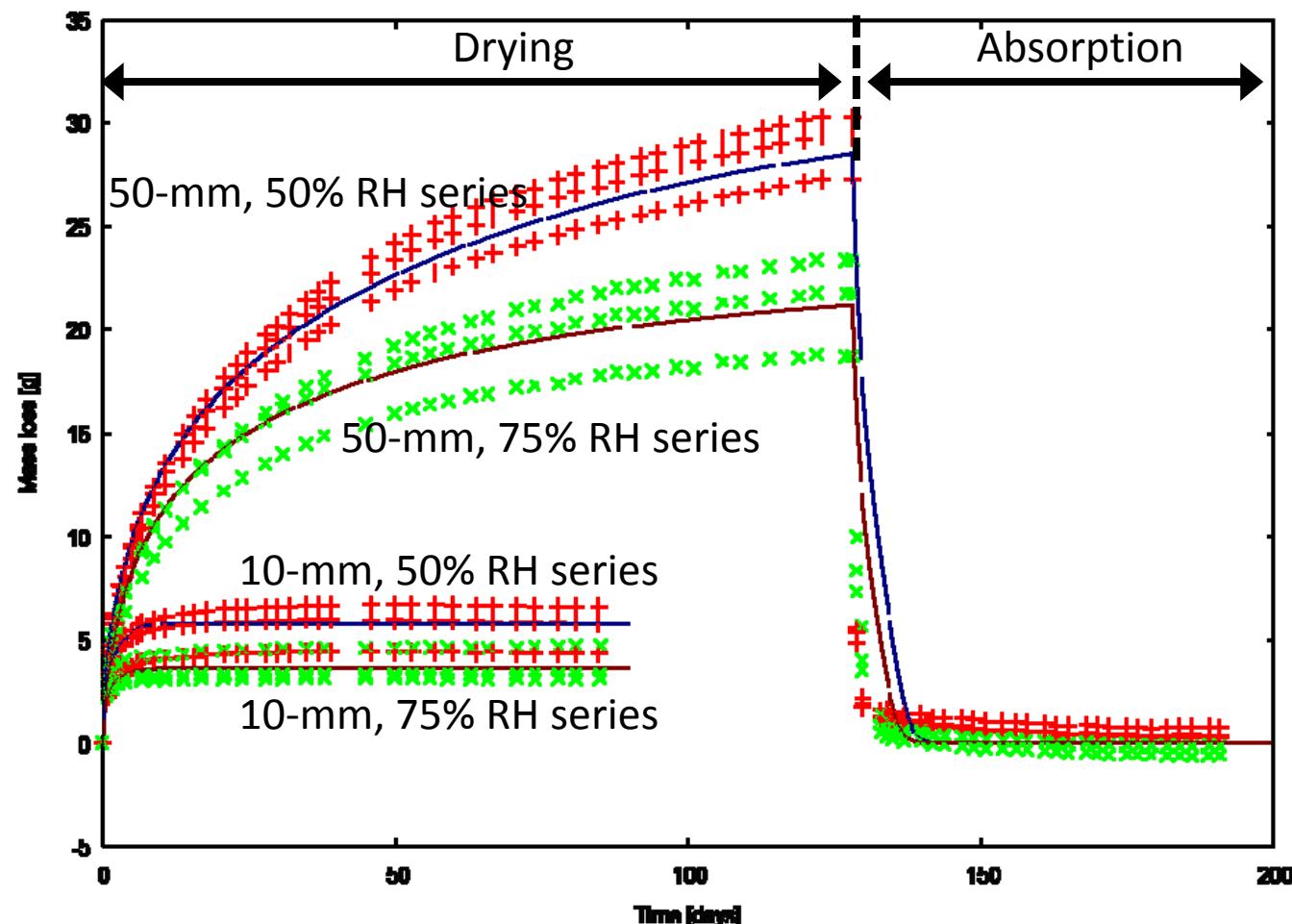
$$\left(\frac{\partial w}{\partial H} \frac{\partial H}{\partial t} + \frac{\partial w}{\partial T} \frac{\partial T}{\partial t} - \operatorname{div}(D_{mH} \operatorname{grad}(H) + D_{mT} \operatorname{grad}(T)) \right) = 0$$

$$S = \frac{1}{\beta(H^\delta - 1) + 1}$$

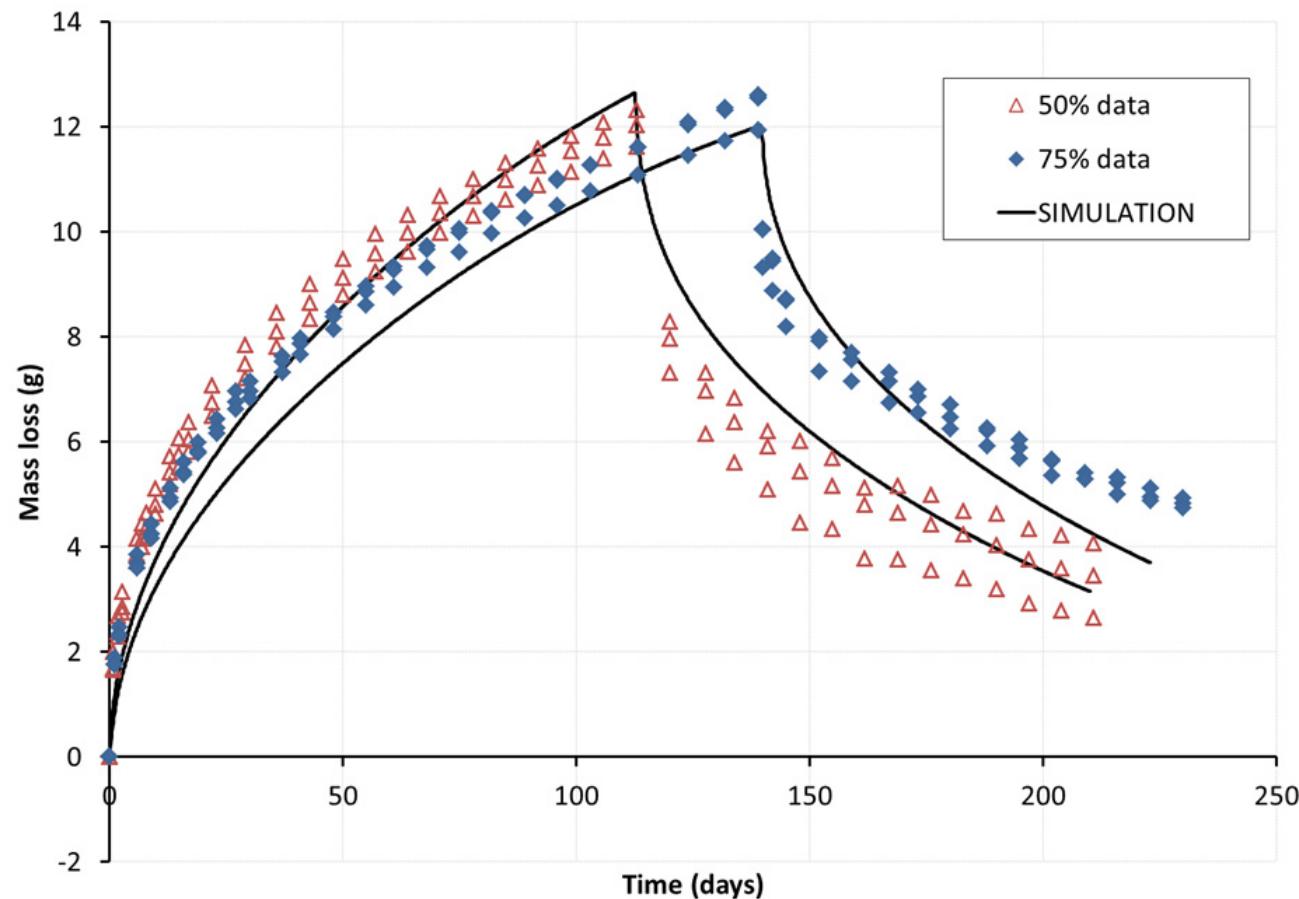
$$D_{mH} = \frac{k_s k_r^l \rho_l R T}{\mu M_w H} + \frac{D_v^o \tau_s \tau_r^g M_w p_v^s (\phi - w)}{\rho_l R T}$$

$$k_r^l = \frac{1}{1 - a + aS^b}$$

0.65 w/c opc concrete



0.40 w/c opc concrete + dampproofer



The transport of ions in **STADIUM** is modeled using the extended Nernst-Planck equation with an advection and temperature term:

Mass conservation equation: $\frac{\partial(wc_i)}{\partial t} + \text{div}(\mathbf{j}_i) = 0$

Flux of ions:

$$\begin{aligned}\mathbf{j}_i = & -D_i w \text{grad}(c_i) - \frac{D_i z_i F}{RT} w c_i \text{grad}(\psi) - D_i w c_i \text{grad}(\ln \gamma_i) \\ & - \frac{D_i c_i \ln(\gamma_i c_i)}{T} w \text{grad}(T) - c_i \boldsymbol{v}_l\end{aligned}$$

Variables:

- Concentrations c_i
- Diffusion potential ψ
- Relative humidity H
- Temperature T

To complete the system of equations, the following relationships are considered:

Poisson: $\operatorname{div}(\tau w \operatorname{grad} \psi) + \frac{F}{\epsilon} w \left(\sum_{i=1}^N z_i c_i \right) = 0$

Heat conduction: $\rho C_p \frac{\partial T}{\partial t} - \operatorname{div}(\kappa \operatorname{grad}(T)) = 0$

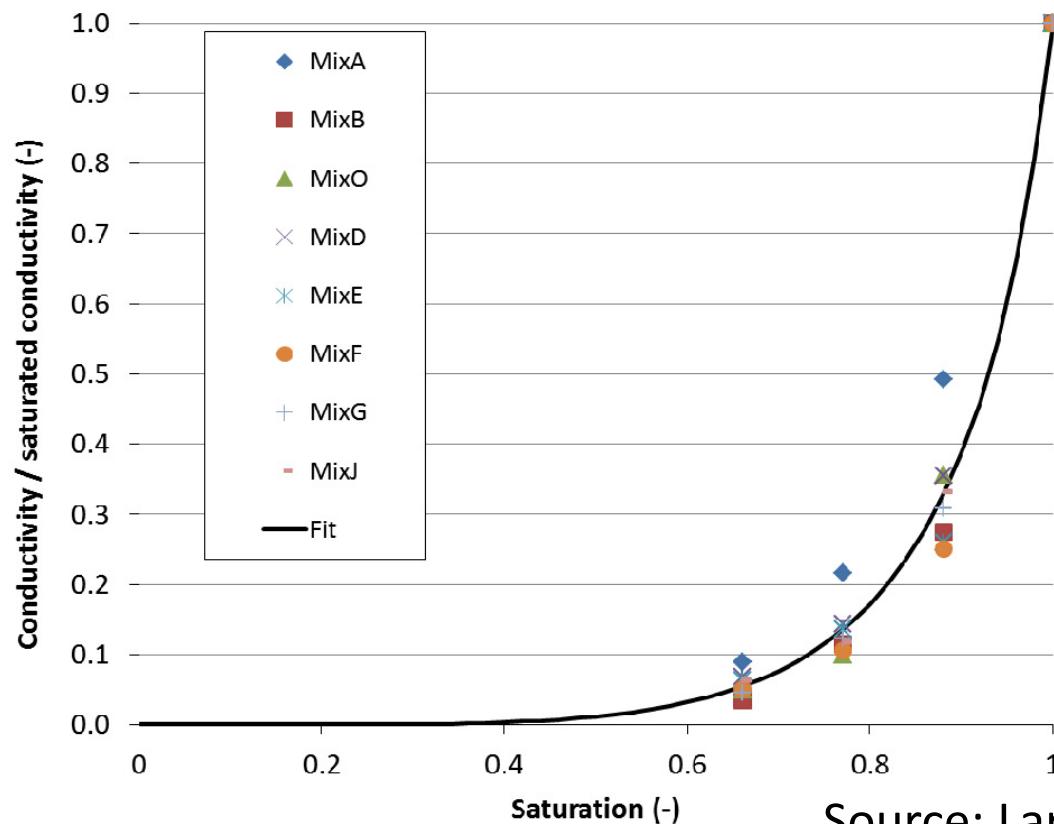
The system of equations is solved using the finite element method:

- N+3 unknowns:** $N \times c_i + H + \psi + T$
- N+3 equations:** N conservation + Poisson + moisture + Heat

Diffusion coefficient: $D_i = \tau_s \tau_l^r D_i^o$

- τ_s : intrinsic tortuosity
- τ_l^r : relative tortuosity
- D_i^o : self-diffusion coefficient = $f(T)$

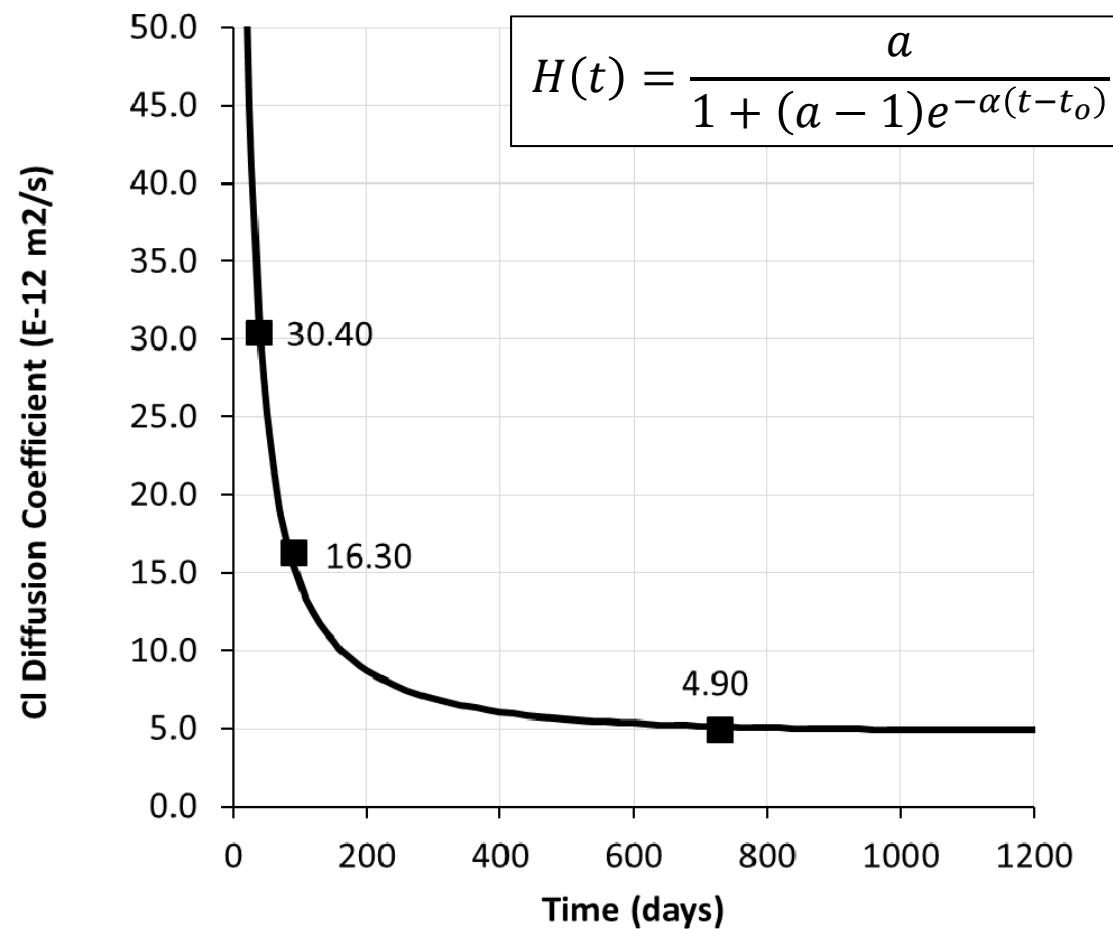
Effect of saturation on tortuosity:



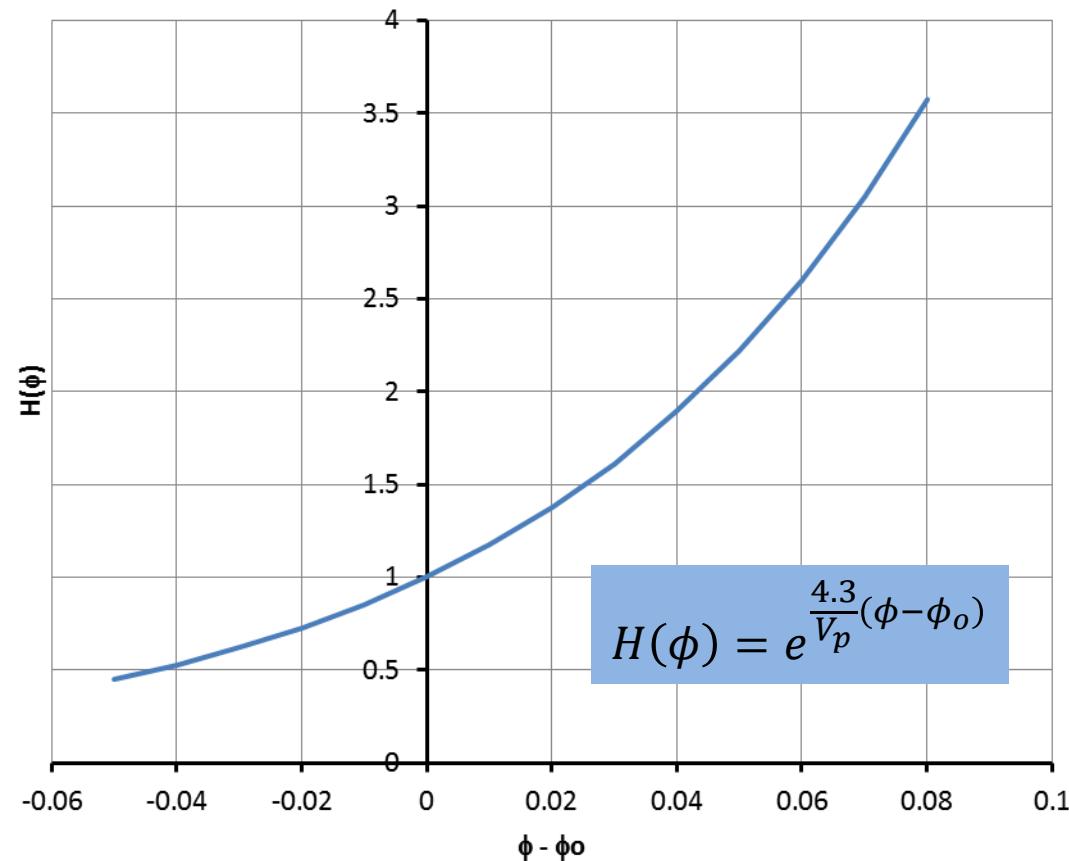
$$\tau_l^r = \frac{D(s)}{D_{sat}} = \frac{\sigma(s)}{\sigma_{sat}}$$

Source: Larsen et al., RILEM pro-051 2006

Effect of hydration on tortuosity:



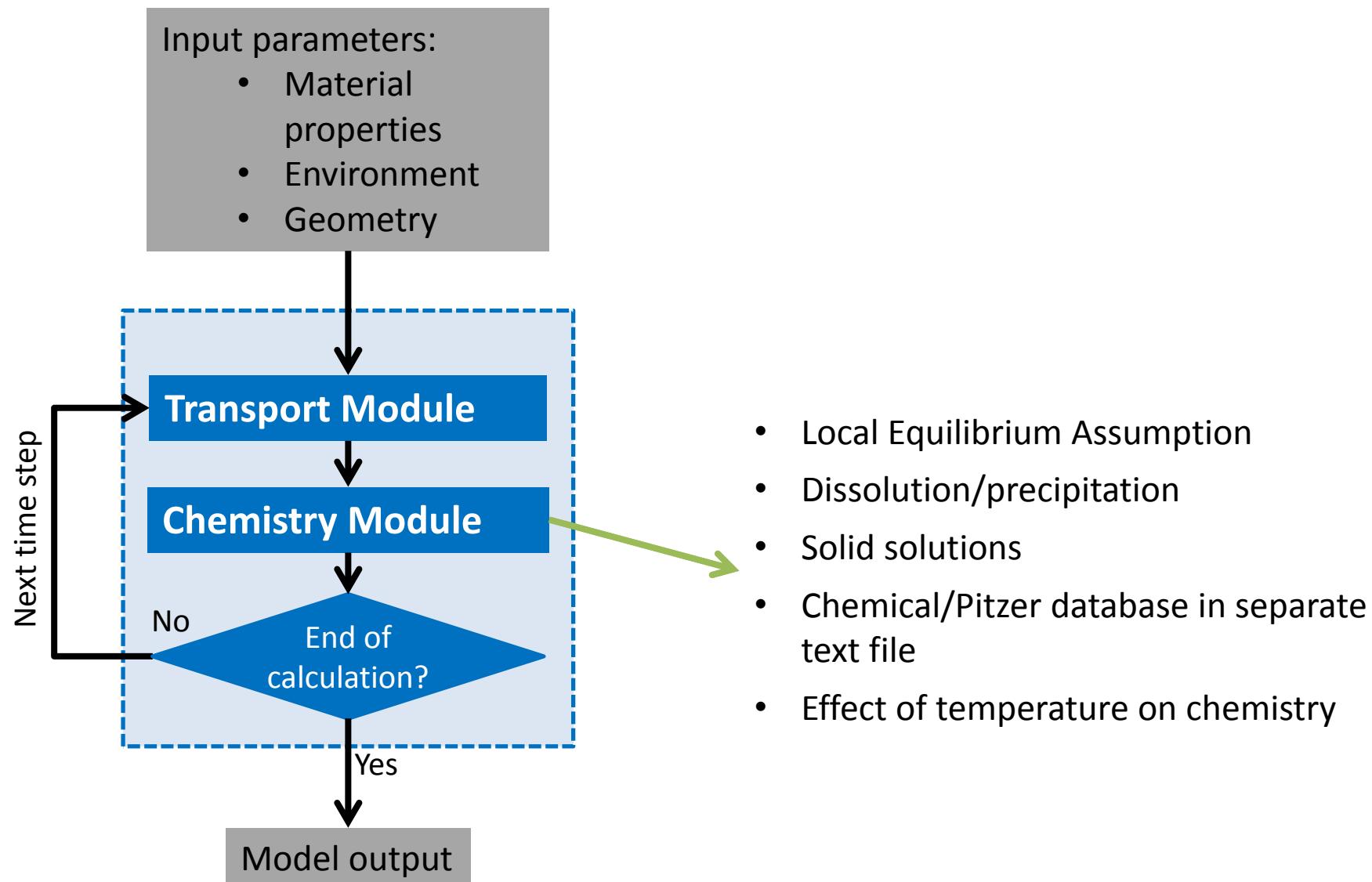
Effect of dissolution/precipitation on tortuosity:



Mechanisms	Properties	Lab tests
Electrodiffusion of species	Diffusion coefficient	Migration test
	Porosity	ASTM C642
Moisture transport (liquid & vapor)	Permeability	Drying test
	Moisture isotherm	Drying test
Heat conduction	Thermal conductivity	Estimated
	Heat capacity	Estimated

Numerical methods:

- All equations are coupled to each other (e.g. temperature influences moisture and diffusion),
- The equations are solved using FEM,
- 1D and 2D versions are available.
- Euler implicit time-stepping.
- Adaptative time-stepping.



The chemical reactions are modeled according to dissolution/precipitation equilibrium relationships:

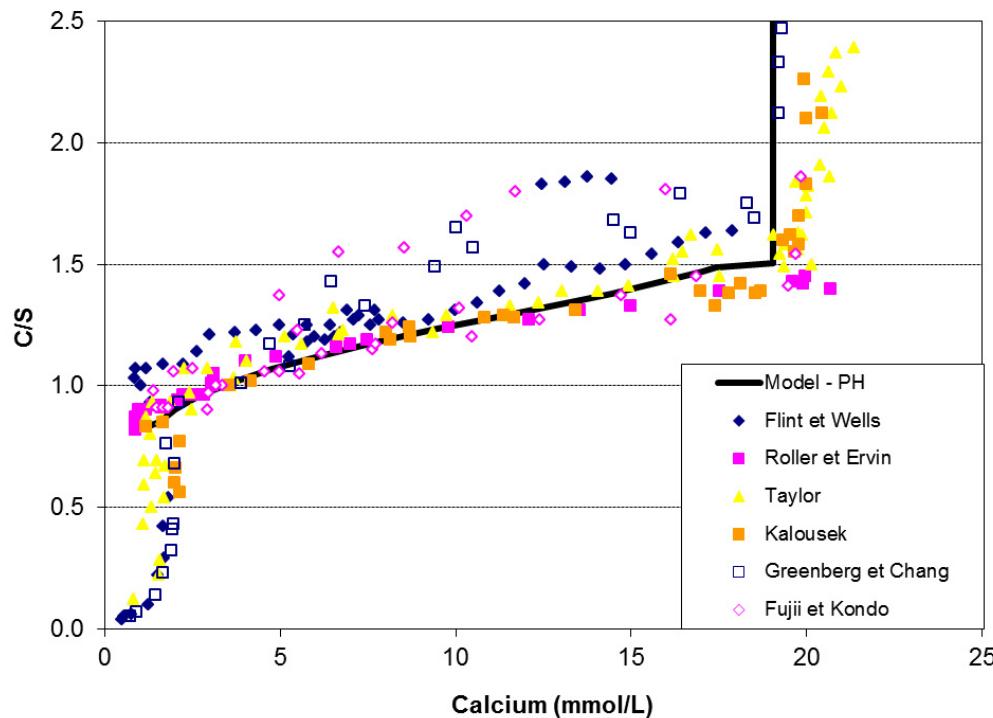
- **Dissolution/precipitation:** $K_m = \prod_{i=1}^N c_i^{\nu_{mi}} \gamma_j^{\nu_{mi}}$ with $m = 1, \dots, M$

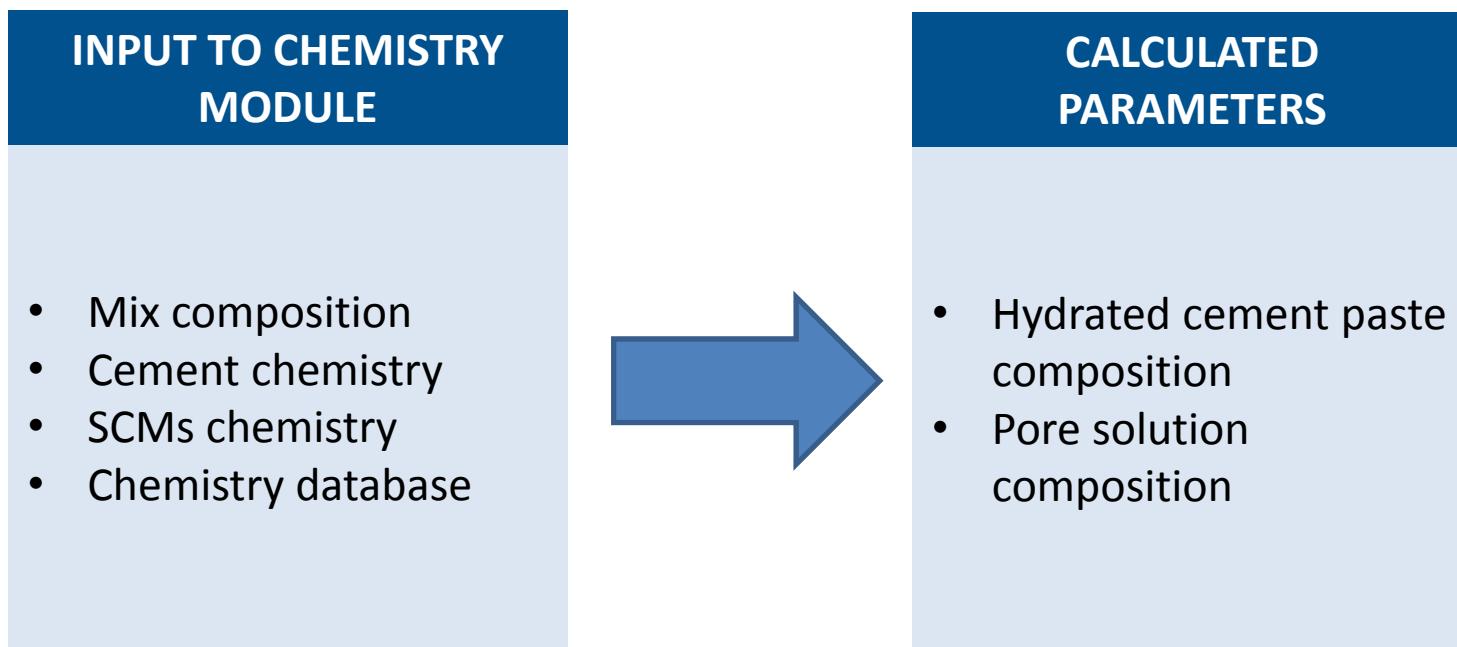
In the case of chlorides, the formation of Friedel's salts is modeled according to an ionic exchange relationship:

- **Friedel's salts formation:** $\underbrace{[\text{AF}_m^+ - \text{SO}_4^{2-}]}_{\text{monosulfates}} + 2\text{Cl}^- \rightleftharpoons \underbrace{[\text{AF}_m^+ - 2\text{Cl}^-]}_{\text{Friedel's salt}} + \text{SO}_4^{2-}$
- **Relationship:** $K_{\text{Cl}/\text{SO}_4} = \frac{\{\text{Cl}\}^2}{\{\text{SO}_4\}} \frac{[\text{AFm}_{\text{SO}_4}]}{[\text{AFm}_{\text{Cl}}]}$

C-S-H model:

- Berner's approach: C-S-H \longrightarrow $\text{CaH}_2\text{SiO}_4 + 1.65 \text{ Ca(OH)}_2$
- $K_{ps} = f(C/S)$ for CaH_2SiO_4 and Ca(OH)_2





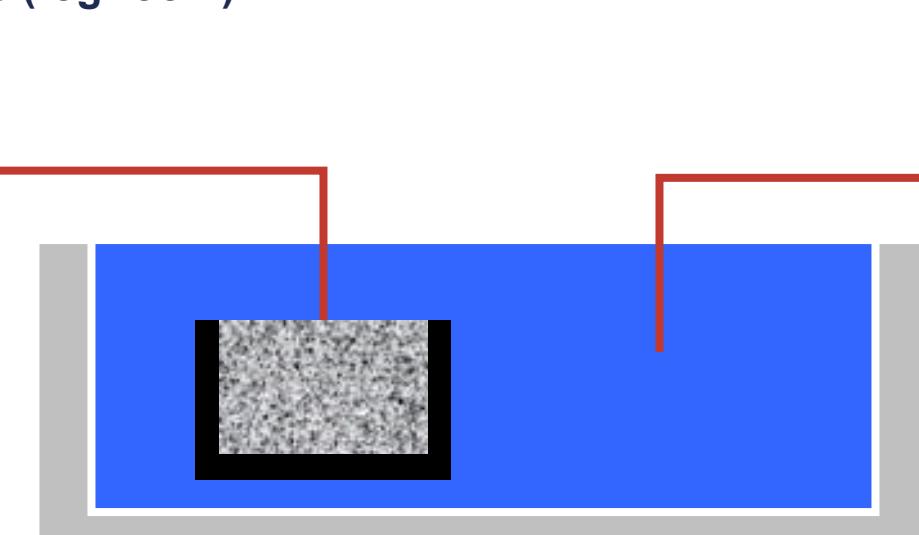
At the end of calculations, the model provides the following information:

- Space and time distribution of species concentrations,
- Space and time distribution of mineral contents,
- Space and time distribution of temperature and humidity,
- Analysis of the main variables to get: total calcium, sulfur and chloride content.
- Space and time distribution of pH.
- Chloride content at specific depth to estimate the time to initiate corrosion for different rebar depths.

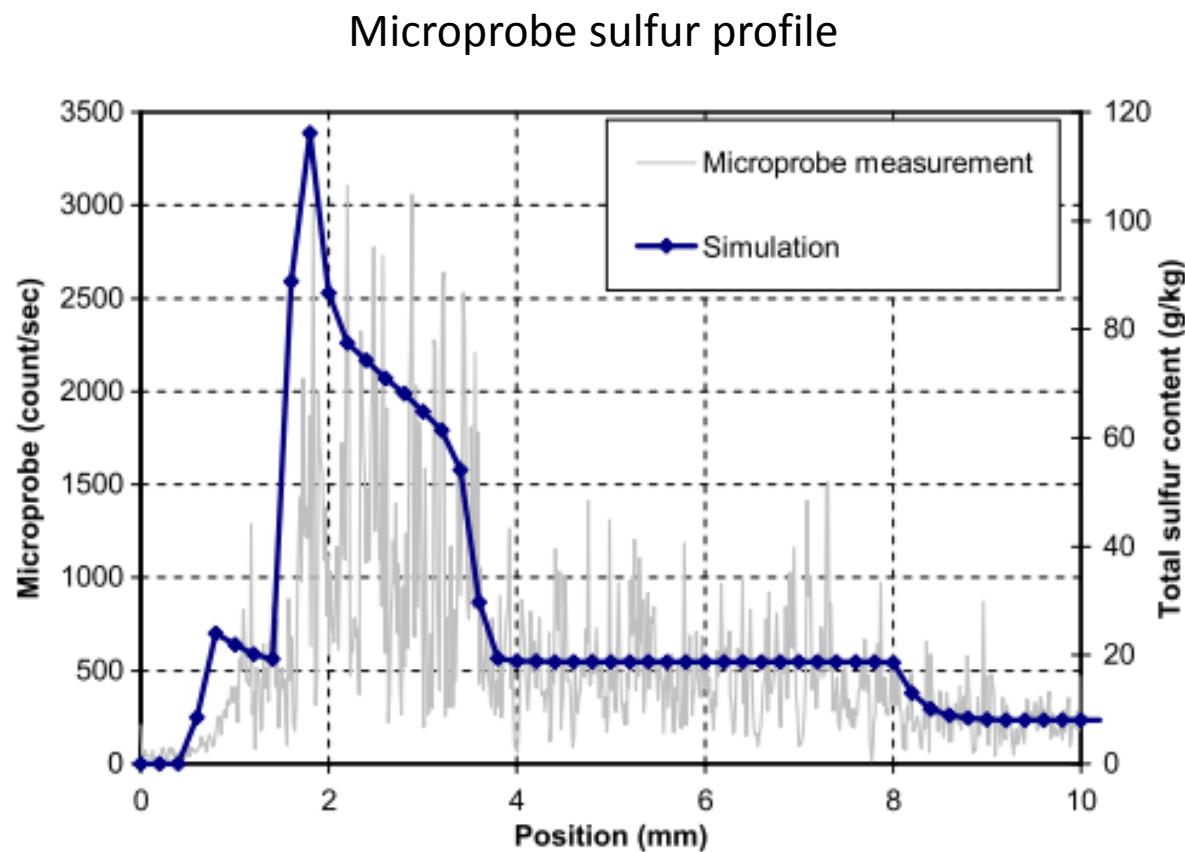
Sulfate exposure

- Paste sample
- Thickness: 25 mm
- Sealed except on top
- Hydration: 28 days (fog room)

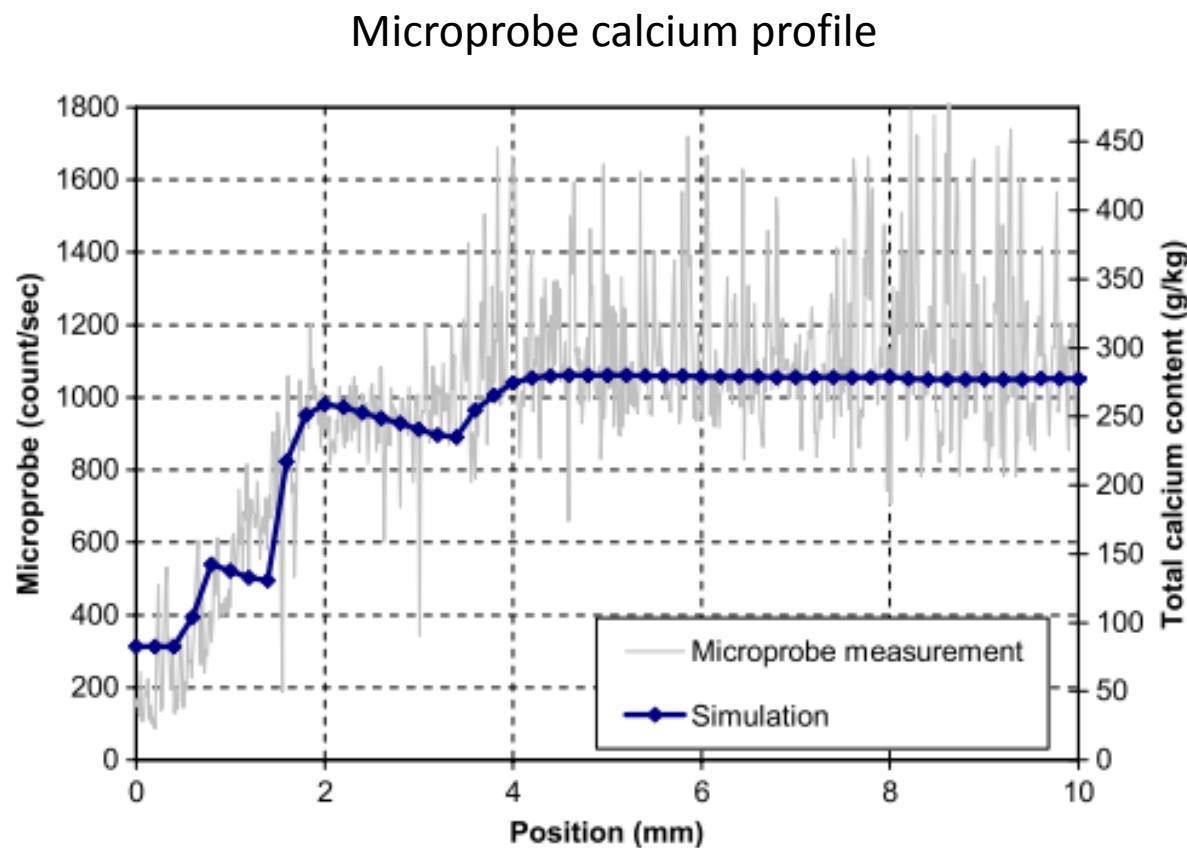
- Volume of solution: 30 L
- Regularly renewed to maintain stable conditions
- Exposure duration: 12 months
- Solutions: 50 mM Na₂SO₄



Sulfate exposure

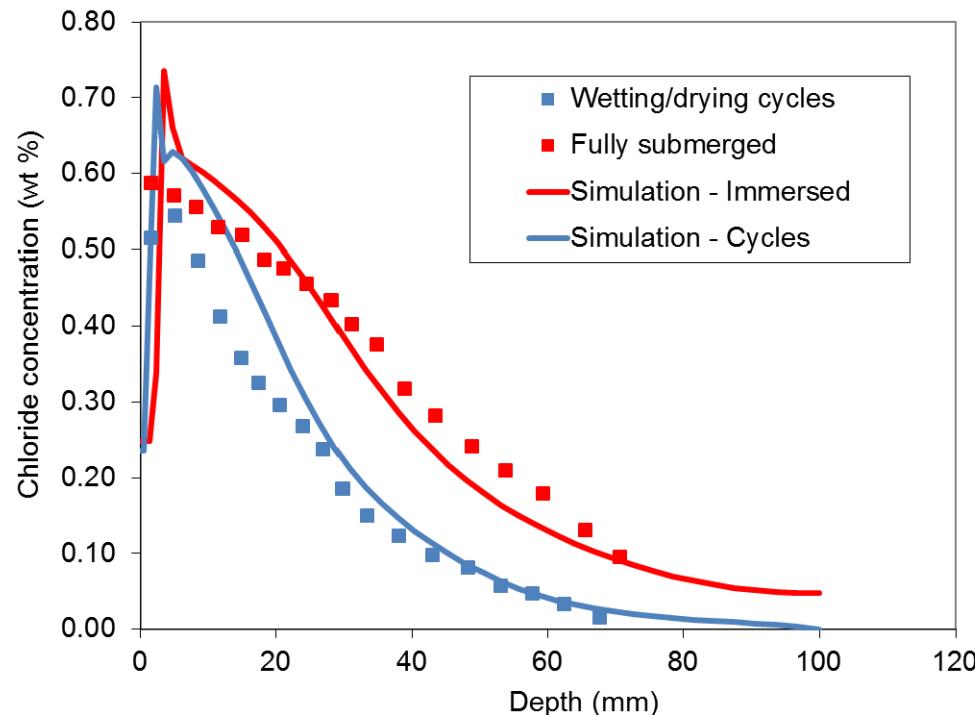


Sulfate exposure

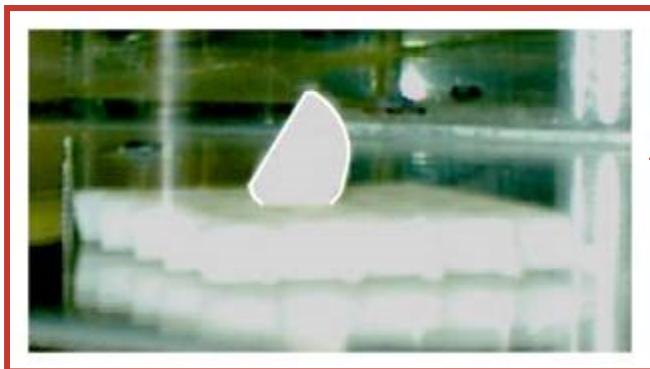


Chloride profiles: wetting/drying cycles vs. immersed

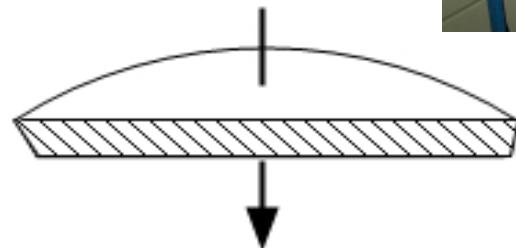
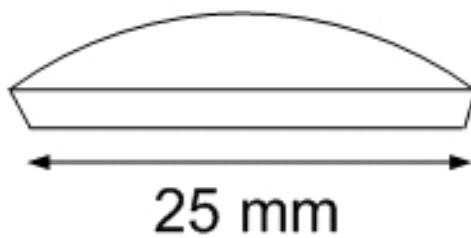
- Solution: 0.5 M NaCl
- Cycles: 3 days in solution, 4 days drying at 50% RH
- Duration: 2.5 years



C3S paste exposed to pure water

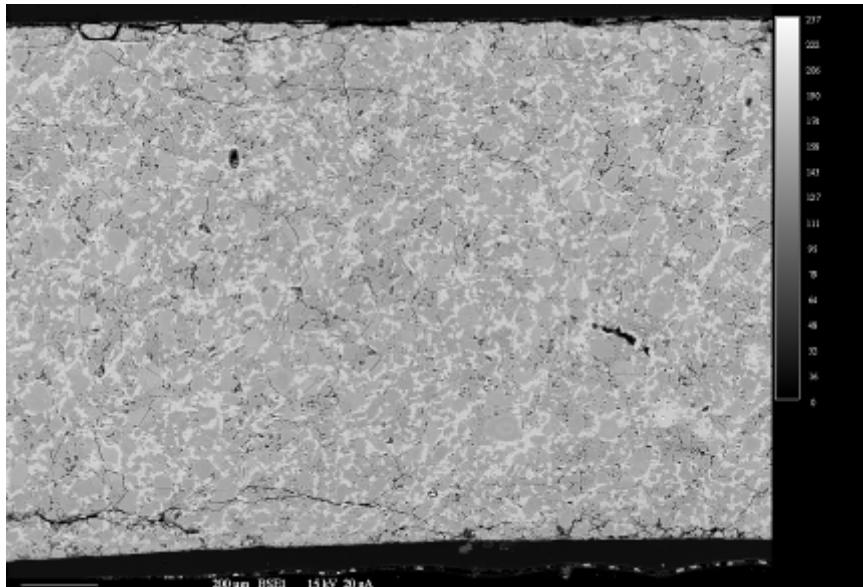


25 L Tank

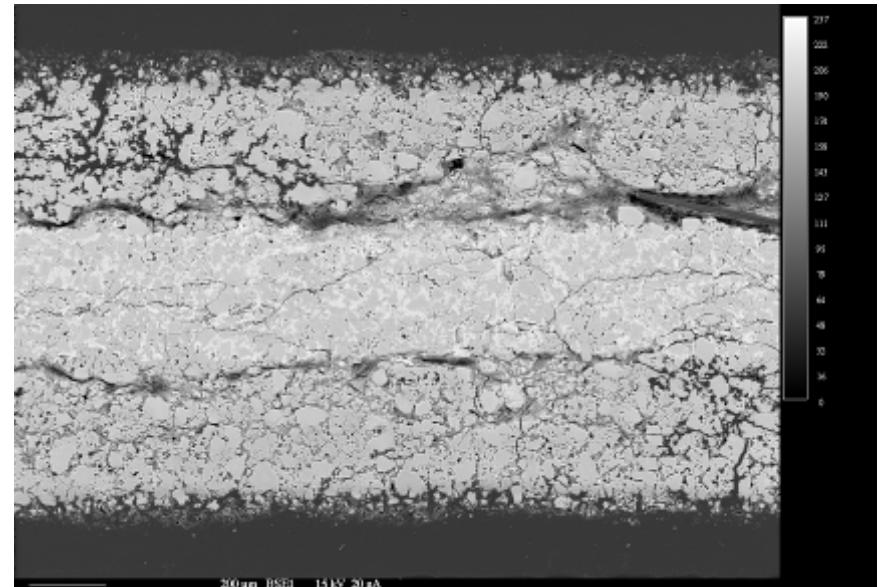


C₃S paste exposed to pure water

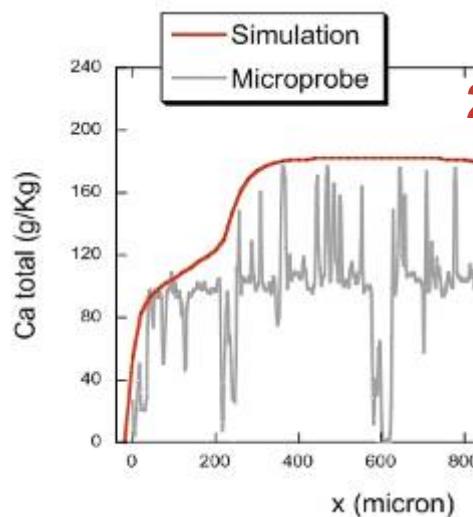
Sound C₃S paste



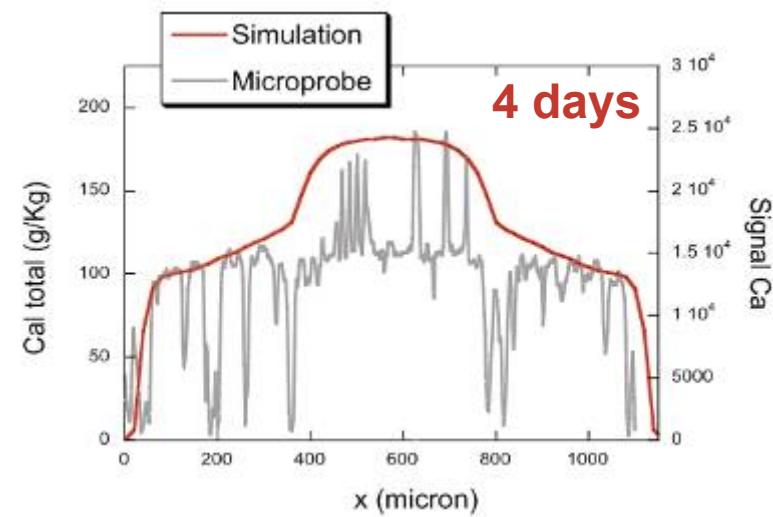
Leached C₃S paste



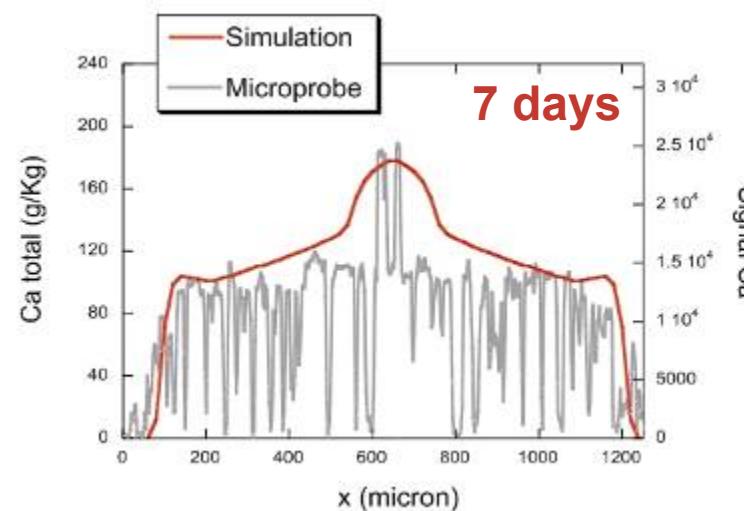
C3S paste exposed to pure water – Ca profiles



2 days

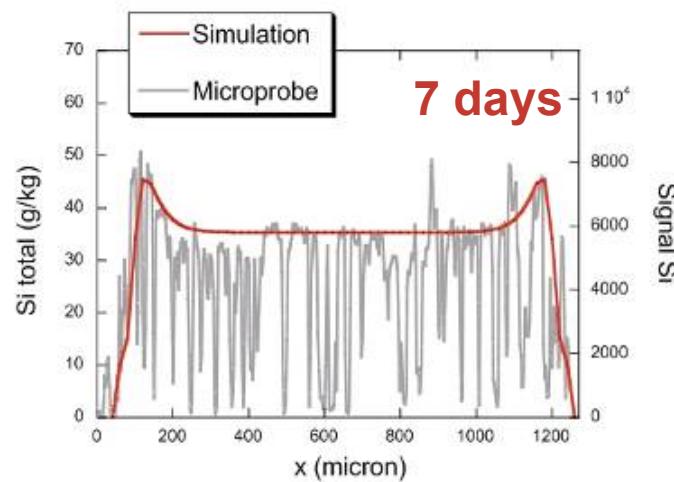
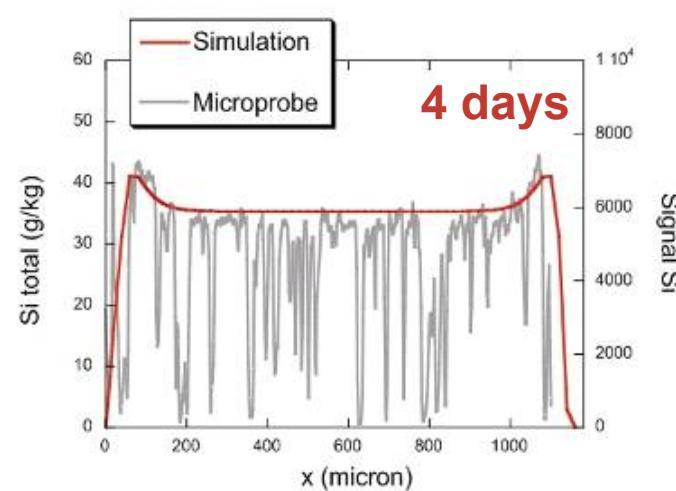
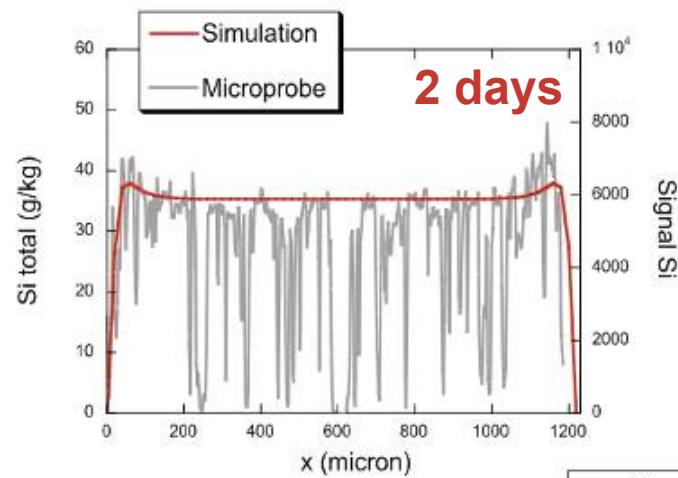


4 days



7 days

C3S paste exposed to pure water – Si profiles





Questions?